

of the European Federation of EPR groups on Advanced EPR

Outline:

- Rapid Scan (RS) EPR introduction
- RS signal simulations
- RS signal deconvolution algorithms
- Instrumentation
- Applications
- Summary

Rapid Scan (RS) EPR has been many things ...

Continuous-wave (<u>CW</u>) Magnetic Field Scan EPR:

- Old Bruker RS (50 & 200 G) => Fast scan
- Linear scan NARS, including segmented (Hyde lab)
- Triangular RS, including segmented (Eaton lab)
- <u>Sinusoidal scan (Eaton lab)</u>

Frequency rapid-scan (1970th NMR) (2010th EPR) (not for today)

CW method has been evolving to become many. Terminology is confusing. Two major factors that distinguish 'Rapid Scan' CW methods:

A) Magnetic field function of time, B(t), vs. EPR spectral width, LW.

B) <u>Theoretical model</u> used to transform EPR(t) signals into EPR(B) spectra



Theoretical models for spin system response:

1. 'Slow scan': Memoryless system: Response R(t)=LineShape[B(t)]

$$dB(t)/dt T_2^* < LW = (\gamma T_2^*)^{-1}$$

- 1st harmonic CW
- Multi-harmonic CW
 - NARS
 - 'Slow' RS EPR (short relaxation times)

Data processing is rather straightforward: mapping time to field domain.

2. 'True' rapid scan: Linear time-invariant (LTI) system (with Memory)

LTI: Output(t) = Input(t) \otimes impulse_response(t)

Full-scan (linear and sinusoidal) EPR
 Standard CW, long T₂ => distortions

Passing resonance at t_0 R(t > t_0)

 $dB(t)/dt T_2^* > LW = (\gamma T_2^*)^{-1}$

My today's RS EPR is:

- Sinusoidal scan
- Magnetic field scan covers the entire EPR spectrum



• Spin system approximates as a linear time-independent system (LTI)

What is the advantage of using the LTI rapid scan model? <u>It is EPR sensitivity enhancement</u>.

Big picture description first, more details later ...

For spins, fast transition through the resonance is equivalent to a pulse Short pulse at high power => larger tipping angles => stronger signal As in FID EPR, there is no spin saturation at high scan rate (short pulse)

LTI RS EPR vs. FID & echo EPR

- Both perform better if relaxation times are long
- No dead-time for RS, but LNA protection is problematic (more later)
- RS is bandwidth limited only due to Q-factor (more details later)
- No spin echo for RS (yet)

Again, RS EPR logic:

- Faster scan rates => Reduced saturation & Large B₁
- Because linear model and by definition => Signal grows $\propto B_1$



A discrete set of resonance frequencies can be achieved by using a switchable capacitors bank



Example: Our 3D printed box with a PCB inside permits six frequencies from 9 to 27 kHz

LTI RS Theory

Linear system is uniquely described by an impulse response function:

$$x(t) \rightarrow \qquad h(t) \qquad \rightarrow \qquad r(t) = x(t) \otimes h(t) \qquad \qquad a x(t) \rightarrow a r(t) \\ x(t+\tau) \rightarrow r(t+\tau) \\ R(\omega) = X(\omega) H(\omega)$$

In (small angle) pulsed EPR, h(t)=FID(t) and x(t)=B₁(t). EPR spectrum: H (ω) = R(ω) / X(ω) < = Deconvolution Often X(ω) X*(ω) = 1 => H (ω) = R(ω) X*(ω) not an ill-posed problem

EPR example, Frank Sequence

Paper link: https://www.ncbi.nlm.nih.gov/pmc/articles/PMC3107679/



$r(t) = x(t) \otimes h(t)$

r : EPR signal h : FID

 $R(\omega)=X(\omega) EPR(\omega)$

Figure 1

The pulse sequence that was used to produce the spectra in <u>Figure 2</u> consisted of 256 pulses of 109 ns with the 16 different phases selected as shown in part a. The time required for the complete sequence was about 56 μ s. The detailed timing of the first 2 and last 2 pulses is shown in part b. Data were acquired continuously at 4 ns intervals during the entire pulse sequence, but only the signal corresponding to times between the pulses was analyzed.

Author Manuscript

Before looking into RS EPR data processing

let's see how to compute RS EPR signal for spin 1/2 system?

Approach 1.

Straightforward but time consuming way is to solve the Bloch Equations.

function dM = RSS	(t,M,par)				
gamma=1.7608e7; 🖇	rad s-1 G-1				
88	%				
Bl=par.Bl; Vm=par.	.Vm; hm=par.	hm; dH=par.	dH; T2=par.T	2; T1=par.T1;	
8 8					
wy=0;					
wx=gamma*Bl;					
WF=-cos(2*pi*Vm*t);					
A=gamma*(dH+0.5*hm*WF);					
8	%				
dM = zeros(3,1);	% (x,y,z)	a column ve	ctor		
M0=1;					
% M1	M2	M3	MO		
dM(1) = -M(1)/T2	-A*M(2)	+wy*M(3)	+0;		
dM(2) = +A*M(1)	-M(2)/T2	-wx*M(3)	+0;		
dM(3) = -wy*M(1)	+wx*M(2)	-M(3)/Tl	+M0/T1;		

It may take several cycles to get a steady-state solution



Approach 2.

Solve directly for steady state solution

Differential become algebraic equations

Much faster computation based on inversion of five-diagonal matrix.

EasySpin Documentation Publications Website Forum

Rapid scan: Steady-state solution of the Bloch equations

This user guide explains how to calculate steady-state solutions of the Bloch equations for a spin-1/2 in the presence of field modulation, using EasySpin's function blochsteady. This forms the basis of Rapid-Scan EPR.

This user guide contains the following topics:

- · Time-domain cw EPR signal
- Some options
- Field sweeps
- · Powder averages

Keep in mind that blochsteady is a new function as of EasySpin 5, and it will likely change and expand in future releases.

Our MATLAB version with examples from www.TseytlinLab.com

Link to MATLAB RS EPR demonstrations, including GUI app

https://www.tseytlinlab.com/we-share



DemoWithComparison.m: major program to run

When run simulations, you should notice some important details: Two RS signals per period.



During scan, two time periods can be very roughly distinguished: Passing through resonance (strong interaction with B_1)

Escaping from the resonance (very weak interaction with B_1)



Scan rate increase: Absorption/Dispersion --> FID - like signal



RS is in-between CW and pulse!

par.hm=5;	010	Bpp modulation amplitude [G]
par.dH=0;	010	Offset from central field position [G]
par.T1=2e-6;	0/0	T1 [s]
par.T2=2e-6;	010	T2 [s]
par.B1=0.01;	00	B1 field [G]

More nuances: accelerating oscillations?



RS EPR signal is measured in the constantly changing magnetic field B(t)

\\\\\\\



For comparison Slow Scan EPR...



RS signal bandwidth & its estimation

B(t) = 0.5 B_{pp} sin($2\pi f_s t$), where f_s is scan frequency Highest rate is at t = 0, and equal to rate_{max} = $\pi B_{pp} f_s$ During 5T₂* ring-down time, the Larmor frequency will change by: $\Delta \omega_L = \gamma \Delta B \approx \gamma rate_{max} 5T_2^* = \gamma 5\pi B_{pp} f_s T_2^*$ Bandwidth estimates as $2 \Delta f_L = \Delta \omega_L / \pi = -\gamma 5 B_{pp} f_s T_2^*$ must be $< f_0 / Q$



Back to LTI RS Theory: Data Processing

Any linear system is uniquely characterized by an impulse response function:

$$x(t) \rightarrow h(t) \qquad \rightarrow r(t) = x(t) \otimes h(t) \qquad a x(t) \rightarrow a r(t) \\ x(t+\tau) \rightarrow r(t+\tau) \\ \hline R(\omega) = X(\omega) H(\omega) \\ \hline R(\omega) = X(\omega) \\ \hline R(\omega) \\$$

Detected_signal(t) = $B_1(t) \otimes FID(t)$

- CW RS EPR (B_1 = const) => deconvolution as-is does not work
- FT(const) = const * $\delta(\omega)$

In principle, RS signals can be fitted as is. However, not very practical

(Absorption) EPR spectra can be obtained in two major steps: Step 1. Transformation into the frame reference of the Larmor frequency

$$x(t) = B_1$$
$$B_0 = B_0(t)$$
$$r(t)$$

$$f(t) = \exp\{-j \phi(t)\}$$

$$\phi(t) = \gamma \int B_{\rho}(t) dt$$

$$x(t) = B_1 f(t)$$
$$B_0 = const$$
$$r'(t) = r(t) f(t)$$



In the new accelerating frame:

- Larmor frequency does not accelerate
- **B₁(t)** vector becomes time-dependent

Field sweep mathematically transforms into frequency sweep!

Step 2. Deconvolution

R'(ω)=X(ω) H(ω)EPR (ω)= H(ω) = R'(ω)/X(ω)

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R'(\omega) = FT (r'), r' – RS signal after transformation
X(\omega) = FT (x), x - B<sub>1</sub>(t) in the new frame
H(\omega) = FT (h), h - FID
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MATLAB real-time demonstrations

MATLABGUI app can be downloaded from

https://www.tseytlinlab.com/we-share



Suggested exercises:

<u>https://www.tseytlinlab.com/we-share</u>

- 1. RUN Simulation, Step1, Step2 using default parameters
- 2. Increase Scan Amplitude to 10, again Run & Step 1 & Step 2
- 3. Increase T₂ to 8000, Run, Step1, Step2
- 4. Scan Frequency to 1000, Scan Amp to 3, ...

Observe transitions: Absorption/Dispersion <-> FID-like signals

- 1. Increase B1 to 40 mG. Observe broadening
- Increase Scan Frequency to 15000. Observe EPR line narrowing
 Do your own simulations,
- Observe RS physics & limitations of this algorithm

The most recent version of the LTI algorithm (2017)

https://www.sciencedirect.com/science/article/pii/S1090780717301635?via%3Dihub



Journal of Magnetic Resonance Volume 281, August 2017, Pages 272-278

Get ri

Full cycle rapid scan EPR deconvolution algorithm

Some limitations still remain:

- Spin system is linear (obvious)
- Periodicity constraint: longest FID duration equal to the scan period
- Reliably removes 1st and 2nd background harmonics, higher problematic
 Why/what is background?
- Scan magnetic field coils in the external magnetic field are essentially single frequency speakers. Vibrations modulate power reflection/transmission to produce EPR-like periodic signals. The highest is the fundamental harmonic.

MATLAB code has a number of 'cleaning' features, such as background removal due to the Microphonic Effect

1st harmonic microphonic, speakers



Force $\propto B_0 B_s \cos \omega_s t$

2nd harmonic microphonic



Force \propto (B_scos ω_s t)² \propto cos 2 ω_s t



Up-field and down-field scans are separated in the ω -domain!



Background removal algorithm

- Step 1. Fourier transformation of rapid scan signal plus background
- Step 2. Separation of up-field and down-field components.

The result is two frequency domain signals.

- Step 3. These two signals are Inverse Fourier transformed into the time-domain
- Step 4. Background signals are fitted in the areas with no EPR , extrapolated into EPR containing areas and subtracted.

Example: background subtraction procedure to spectra of BMPO-OOH at X-band.











CW^{1h} vs. RS vs. FID

1^{st} harmonic CW = CW^{1h}

No dead time, no bandwidth (BW) limit, lower SNR

RS No dead time, Q-limited BW detection, higher SNR with higher CW power, however LNA saturation.



Dead time, Q-limited BW detection & excitation Pulse length limited excitation Signal detected in 'silence' after dead-time



Most straightforward approach: directly compare signal-to-noise (SNR) ratios However, not very informative: you cannot compare SNR of different shapes



A meaningful quantitative approach is to focus on the information

An example: a single Lorentzian line + noise is measured



This line is uniquely defined by two parameters:

- 3. We will not consider phase
- A meaningful question (vs. SNR): what is the uncertainty to measure A and Lw? \bullet
- Same questions can be asked about the derivative line ullet
- Comparison can be made base on the uncertainties in A and Lw. •
- Interestingly, a relation between SNR and uncertainties can be found \bullet
 - Analytically for some cases Ο
 - Numerically Ο
SNR definition, example for a single EPR line



Uncertainty analysis

Equal SNR = 5 absorption and derivative spectra Results of line fitting:



- Uncertainty (SD) in linewidth measurements are similar
- Uncertainty for integral intensities is > twice as large for derivative.

SNR has to be redefined in terms of the accuracy of measurements!

Tseitlin, et al, Concepts in Magnetic Resonance Part A, V40A, Issue 6, 295-305 (2012)

Signal comparison



Phase sensitive detection

 $2 R_{d} \rightarrow \frac{R_{d} \cos^{2} \omega t = R_{d}/2 (\cos 2 \omega t + 1) = R_{d}/2}{x2 \text{ in SNR definition} => R_{d}}$

 $R_a/R_d \approx 3-5$, depending on the modulation amplitude.

RS signal optimization $(B_1 \neq const)$



F = increase in the signal amplitude due to rapid scan

Experimental noise (is not white)



e.g.: 20 kHz => Period = 50 us. EPR spectrum each 25 us. We average 10 – 10'00'000 of RS signals. Averaging of a periodic signal in the time is equivalent to applying a comb filter in the frequency domain

<u>Concept</u>: Averaging of periodic signal.

Time domain: $\sigma \propto 1/(N_{aver})^{\frac{1}{2}}$

Frequency domain comb filter

$$|H(f)| = \frac{\sin \left(N_{aver} \pi f / f_{scan}\right)}{\sin \left(\pi f / f_{scan}\right)}$$



Example: 50 kHz scan frequency & 38 kHz noise component

MMMMM

If noise is white, phase-sensitive detection is $\sqrt{2}$ noise-less vs. direct detection



Fact: Increasing scan frequency does NOT improve SNR

Example:

- A. One CW spectrum with SW=10 G, sweep time 10 s
- B. Two CW same spectra w/sweep time 5 mins. each, spectra are averaged.
- For A and B optimized noise filtering is used
- SNR(A) = SNR(B)
- It is because:
- Faster x 2 means noise x $\sqrt{2}$ but averaging x $1/\sqrt{2}$

<u>Conclusion 1</u> Faster scan doesn't reduce noise if experimental time is const. <u>Conclusion 2</u>: Phase sensitive detection reduces noise $\cong \sqrt{2}$ In practice, a lot will depend on prior amplification stages SNR gain for RS vs. CW^{1h}

Assuming white noise. SNR gain is estimated as $\sqrt{2}$ F R_a/R_d

This or a single EPR line this translates into reductions of uncertainties

For amplitude: $\sqrt{2} F R_a/R_d$

For line width: $2\sqrt{2} F R_a/R_d$

- Up to x100 SNR gain for samples having long relaxation times.
- Spin system saturates at lower powers but the detection system is not.
- More about this issue later ...

Instrumentation: RF/MW units

But before, brief summary of facts we learned and related conclusions:

- RS algorithm requires quadrature signal, both M_x and M_y components.
- Slow scan regime: M_x and M_y are dispersion and absorption, respectively.
- Rapid passage: not any more when FID-like signal
- RS bridge is similar to pulse bridge. In fact, a pulse bridge can be used.
- A limiter may be needed to protect the detection system, depending on power
- Power is CW. However, detection is broadband and limited by the resonator Q.
- Signal is periodic with no gaps in data acquisition (compare to pulsed EPR)
- RS signals have to be real-time averaged, ideally using an FPGA digitizer.
- RS sensitivity comes from increased power without spin system saturation
- However, LNA saturation and source noise (related to power) is a major problem

LNA: low noise amplifier; Q : resonator quality factor FPGA: field programmable gate array ; RF: radiofrequency; MW microwave Let's start with a simplistic RF/MW power diagram



Two Resonator types: R. Reflection type T. Transmission type

Design aspects that we will address:

Non-EPR reflection (R) and transmission
 (T) needs to be minimized to avoid LNA saturation and noise

Noise transformation

I/Q Down-conversion

A/D conversion with real-time averaging Before looking into LNA saturation, a general for spectroscopy problem: Excitation/detection decoupling

Optics, EPR, NMR, sound, ...



Strong excitation

Everyday life example:

We do not see stars (except for the sun) at day time

Approaches to excitation/detection decoupling:

Approach 1. Time-domain decoupling Examples:

Most of the echo-based methods such as radar, pulsed EPR & NMR <u>Requires blocking detection</u> during excitation pulse => dead-time

Approach 2. Frequency-domain decoupling

Example: Fluorescence, later RS EPR example



There is a 3rd approach used in magnetic resonance: 'Critical' coupling (CC) of the resonator to the transmission line. CC is essential for reflection types of resonators



This approach is a narrow-banded (single frequency) decoupling:

- A small deviation from critical coupling leads to RF/MW reflection
- Reflection may saturate LNA and increase noise
- So we back to the problem of invisible at the day time stars

Noise & Reflection resonators





Higher Q => Sharper curve => More reflected noise

Single frequency CW^{1h} vs. broadband RS

CW ^{1h} bandwidth often 100 kHz or less

RS EPR bandwidth matches that of the resonator > 10 MHz



If Q is low and/or EPR frequency is high, signal gain outperforms noise Reflection resonators deliver sub-optimum RS EPR performance Problem of resonator detuning is more severe for RS EPR (high power) Digital auto-frequency control for reflection resonators Tuning mode (100us) – CW mode (50 ms) – Tuning – CW -



Wide tuning BW, 2-30 MHz (trade-off) Do not interfere with RS data acquisition Discrete AFC (DAFC) vs.

Global one-step target search



Standard AC AFC & DC AFC

Local iterative convergence



What happens when the cat loses sight of the mouse?

DAFC in use: Resonator loop is placed on a mouse breast tumor.

AWG frequency time variation during *in vivo* measurements using DACF. DACF tracks mouse breathing that modulates the resonator frequency.

NHW 57.35 57.3 57.25 57.25 57.2 57.2 57.2 57.2							
0	2	4	6	8	10	12	
lime, seconds							

Does not work with the standard first-derivative CW EPR Standard AFC => background, and blurring Transmission mode and 4th decoupling approach it is based on the Faraday's law.

Electromotive force \propto rate of change of magnetic flux through the loop



Bi-modal design (quadrature coils)



Excitation resonator (ER) creates RF/WM magnetic field along y-axis
Detection resonator (DR) tuned to the same frequency is isolated from ER excitation
Spin magnetization rotates in the xy-plane to induce EPR signal in DR



SignalCore source: SC5510A

Sideband	phase	noise ³	(dBc/	Ήz)
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	RF Frequency								
Offset	10	1 GHz		5 GHz		10 GHz		20 GHz	
	typ	max	typ	max	typ	max	typ	тах	
100 Hz	-80	-74	-66	-60	-60	-54	-54	-48	
1 kHz	-122	-116	-108	-104	-102	-96	-96	-90	
10 kHz	-134	-128	-121	-115	-115	-110	-110	-105	
100	-135	-129	-121	-115	-115	-110	-110	-105	
1 MHz	-135	-129	-121	-115	-115	-110	-110	-105	
10 MHz	-150	-145	-139	-136	-133	-130	-131	-130	
FLoor	-152	-145	-150	-144	-147	-145	-145	-145	

Additional advantage of the bimodal design: Stability w/respect to detection resonator de-tuning.

Major challenge: is to keep insolation high enough Locket type resonator developed in our laboratory for RS EPR imaging of mouse breast tumor models:





Flexibility, can be used for CW, RS, pulse.

Arbitrary Waveform Generator BW=120 MHz (up to 200 MHz) Is more than needed

On the detection side: two-step down-converion



This design enables digital AFC (introduced above) at IF frequency





Wide tuning BW, 2-30 MHz (trade-off) Do not interfere with RS data acquisition

Instrumentation: Scan coil/driver

- Implementation RS EPR requires generation of stable sinusoidal scans B(t) = 0.5 B_{pp} sin(2π f_s t + phase)
- To achieve large B_{pp} , coil inductance is resonated with capacitors
- B_{pp} has to be accurately measured and very stable
- Small phase change => time shift (dt) => field shift = dt*scan_rate=> broadening
- One full scan produces two EPR spectra, used for fine phase tuning
- The use of digital feedback control is reliable, also inexpensive More details in next slides....

Digital feedback to control scan amplitude and phase (Coil driver)

CV-1800 1.8 kW audio amplifier BW up to 100 kHz, \$399



'Large' RS coils, 10 cm gap, used for conscience mouse measurements



Tested at to 100 kHz & 12 Gpp

3D printed



Formlabs Form 2 3D Printer \$3,350.00 halve-coil







Rapid Scan (RS) CW EPR: What's Next?



Rapid scan spin echo/ phase cycling



 $M(t) -> B_1(t)$

In the new accelerating frame

- Magnetization phase does not rotate
- Instead, B₁ phase changes with time

Pulse phases is controlled with magnetic field modulation !

Tseytlin M. Z Phys Chem (N F). 2017 Mar;231(3):68

Reference Frame Transformation Enables Phase Cycling



After transformation: $A {\rightarrow} A'$, $B {\rightarrow} B'$



 $\Phi = \begin{pmatrix} phase \ FID_1 \\ phase \ FID_2 \\ phase \ Echo \end{pmatrix} = \begin{pmatrix} -\pi/2 \\ -2\alpha - \pi/2 \\ -4\alpha + \pi/2 \end{pmatrix}, \quad \alpha = \frac{\gamma B_{pp}}{4\pi fm}$

Tseytlin M. Z Phys Chem (N F). 2017 Mar;231(3):68

FM Phase Cycling

 $\Delta \alpha$

Phase cycling requires two measurements with different $\alpha = \frac{\gamma B_{pp}}{4\pi fm}$

Relative phases for the measurement in the accelerating frame: $\Delta \Phi = \begin{pmatrix} 0 \\ 2 \end{pmatrix}$


Second example FM pulsed EPR:

Isolation of the excitation from detection in a bi-modal resonator









ADC

Relaxation times measurement of trityl radical using RS resonator $B_{pp} = 6G$, $f_m = 96$ kHz not sufficient to demonstrate dead-time reduction



L-band, Modulation 480 kHz; FID with 100 ns pulse, 26 MHz de-tuning, Q=100



1. Isolation

2. More importantly, ring-down is 26 MHz away from EPR

Applications in our lab. Functional imaging



EPR oximetric imaging of a mouse breast tumor. (a) Histrogramm of pO_2 distribution. (b) 2D slice of pO_2 image.

First ever /to our knowledge/ real-time PET/EPR co-imaging





https://www.ncbi.nlm.nih.gov/pubmed/29676283

Tseytlin et al. Phys Med Biol. 2018 May 16;63(10)

First clinical <u>RS EPR</u> measurements using OxySpot Dartmouth, August 2017

Observed pO₂ reduction & measurement time a few milliseconds









1.4. Imaging of Enzyme Activity by Electron Paramagnetic Resonance

Phosphatase-sensitive Nitroxide spin probe:



X-band EPR spectra of 200 μ M **1** measured at 37°C in 10 mM Tris, pH=7.5, (A) before and (B) 50 min after incubation with 0.08 U/mL ALP, (C) Time evolution of the low-field EPR component.

U. Sanzhaeva; X. Xu; P. Guggilapu; M. Tseytlin; V. Khramtsov; B. Driesschaert, Angew. Chem. Int. ed. 2018, 57(36):11701-11705.

In vitro Proof of Concept using a home made Rapid Scan Scanner (800 MHz)



U. Sanzhaeva; X. Xu; P. Guggilapu; M. Tseytlin; V. Khramtsov; B. Driesschaert, Angew. Chem. Int. ed. 2018, 57(36):11701-11705.

Summary:

- RS (as of today) is an sensitivity-enhanced version of CW^{1h} EPR
- Narrowband CW excitation & broadband detection (as in pulse)
- Most of SNR gain comes using high power & fast scans
- Spin system remains linear (no saturation)
- No dead time
- However, high CW power may saturate the detector (LNA)
- Scan limitations (so far): Up-scan non-overlaps with downscan
- Signal BW grows with scan rate => Q-factor becomes a

RS EPR is good for/when:

- ✓ High conversion power into B_1 . e.g., small resonators
- Long relaxation times & inhomogeneous broadening
- ✓ High field EPR due to larger bandwidth

We use RS EPR for imaging. In comparison with pulsed EPR imaging

- Again, no dead-time (DT). Important if T2 \cong TD, which may happen in the case of O₂ imaging.
- MUCH LESS bandwidth limited. As a result, multi-line multifunctional spin probes can be used.
- Spectral-spatial imaging is used / see lecture by Dr. Boris